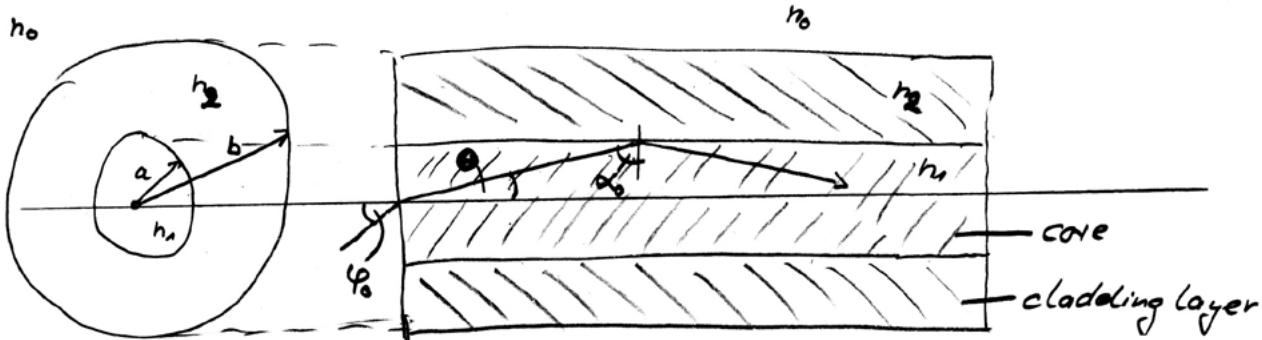


(73)

Optical Fibers



In order to get total internal reflection at the interface Core - cladding we require $n_2 < n_1$

$$\hookrightarrow \text{critical angle: } \sin \alpha_0 = n_2/n_1$$

In order to launch light from outside ($n_0 = 1$) into the core of the fiber, the launch angle can be determined according to Snell's Law:

$$\frac{\sin \varphi_0}{\sin \theta} = \frac{n_1}{n_0}$$

$$\hookrightarrow \sin \varphi_0 = n_1 \cdot \sin \theta = n_1 \cdot \sqrt{1 - \sin^2 \theta}$$

$$\text{use } \theta = 90^\circ - \alpha_0 \text{ and } \sin \alpha_0 = n_2/n_1$$

$$\text{to get } \sin \varphi_0 = \sqrt{n_1^2 - n_2^2}$$

The numerical aperture NA of a typical fiber: (core $\approx 10 \mu\text{m}$, Cladding $\phi = 125 \mu\text{m}$)

$$NA = n_1 \cdot \sqrt{2} \Delta \approx 1.46 \cdot \sqrt{2 \cdot 0.003} \approx 0.113 \Rightarrow$$

~ with an acceptance angle ϕ_0 of

$$\sin \phi_0 = NA \approx 0.113 \quad \Rightarrow \phi_0 \approx \underline{\underline{6.5^\circ}}$$

Modes of Propagation of Light in Fibers:

Again: Maxwell equations

$$\left. \begin{array}{l} \nabla \cdot \vec{E} = S/\epsilon_0 \\ \nabla \cdot \vec{B} = 0 \\ \nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \\ \nabla \times \vec{B} = \frac{1}{c^2} \frac{\partial \vec{E}}{\partial t} + \mu_0 J \end{array} \right\} \begin{array}{l} \vec{E} = -\nabla V - \frac{\partial \vec{A}}{\partial t} \\ \vec{B} = \nabla \times \vec{A} \end{array}$$

↳ Wave Equation for dielectric medium

$$\Delta \vec{A} - \frac{1}{\epsilon_0} \frac{\partial^2}{\partial t^2} \vec{A} = 0$$

Optical fiber represented in cylindrical polar coordinates:

$$x = r \cdot \cos \phi, \quad y = r \cdot \sin \phi, \quad z = z \quad (\text{fiber axis})$$

$$\Delta \vec{A} = \frac{1}{r} \frac{\partial}{\partial r} \left[r \cdot \frac{\partial \vec{A}}{\partial r} \right] + \frac{1}{r^2} \frac{\partial^2 \vec{A}}{\partial \phi^2} + \frac{\partial^2 \vec{A}}{\partial z^2}$$

Solution: $\vec{A}_n = (A_r, A_\phi, A_z) \rightarrow (E_r, E_\phi, E_z)$
 (H_r, H_ϕ, H_z)

time dependency

$$A_n = A_n(r, \phi) \exp[i(\omega t - \beta z)]$$

$$\left[\frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{1}{r^2} \frac{\partial^2}{\partial \phi^2} + (k^2 - \beta^2) \right] \cdot A_z = 0 \Rightarrow$$

→ separation of variables:

$$R_z(r, \phi) = R_z(r) \cdot \exp(\pm i \ell \cdot \phi), \quad \ell = 0, 1, 2, \dots$$

↪ $\frac{\partial^2 R_z(r)}{\partial r^2} + \frac{1}{r} \frac{\partial R_z(r)}{\partial r} + (k^2 - \beta^2 - \frac{\ell^2}{r^2}) \cdot R_z(r) = 0$ Bessel Differential Equation

Solutions: $R_z(r) = C_1 J_\ell(h \cdot r) + C_2 Y_\ell(h \cdot r)$, $h^2 = k^2 - \beta^2 > 0$

$$R_z(r) = C_1 \cdot I_\ell(q \cdot r) + C_2 K_\ell(q \cdot r), \quad -q^2 = k^2 - \beta^2 < 0$$

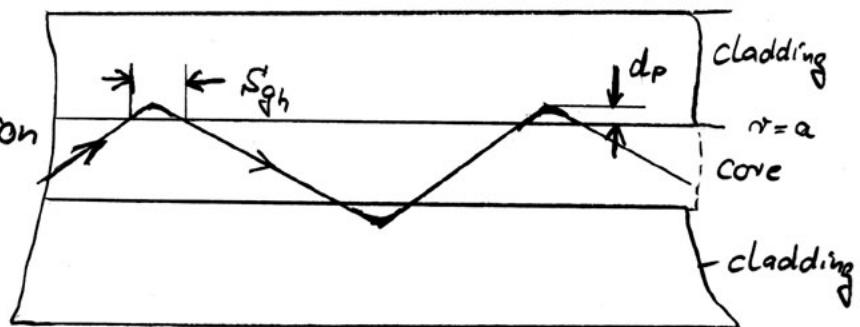
with J_ℓ, Y_ℓ : Bessel functions of first and second kind of order.

I_ℓ, K_ℓ : modified Bessel functions

Boundary Conditions:

Evanescence wave penetration
into cladding layer

leads to



Goos-Haenchen shift S_{gh} and moves effective reflective boundary by d_p into cladding layer. However, the evanescent wave in the cladding must decay exponentially with increasing r . The functions J_ℓ and I_ℓ do not meet this boundary condition: $\Rightarrow \underline{C_1 = 0}$

→ In the cladding layer:

$$E_2 = C \cdot K_e(q \cdot r) \exp\{i(\omega \cdot t + k \cdot \phi - \beta \cdot z)\}$$

$$H_2 = D \cdot K_e(q \cdot r) \exp\{i(\omega \cdot t + k \cdot \phi - \beta \cdot z)\}$$

Since guiding requires $\boxed{\beta > n_2 \cdot \omega/c}$

Continuous tangential field components at $r=a$ can not be met with J_e for finite fields at $r=0 \Rightarrow C_2=0$

↪ Inside core layer:

$$E_2 = A \cdot J_e(q \cdot r) \exp\{i(\omega \cdot t + k \cdot \phi - \beta \cdot z)\}$$

$$H_2 = B \cdot J_e(q \cdot r) \exp\{i(\omega \cdot t + k \cdot \phi - \beta \cdot z)\}$$

Continuous tangential field components for distinct set of propagation constant β_m , $m = 1, 2, 3, \dots$

↪ labeling of modes of propagation

$E H_{0m}$ or $H E_{0m}$

$\boxed{A=C=0}$; for $E H_{0m}$ modes

$\boxed{B=D=0}$ " $H E_{0m}$ modes

i.e., only transverse \vec{E} -component for $E H_{0m} \Rightarrow$ labeled TE_{0M}
 " " \vec{H} -components H_ϕ for $H E_{0m} \Rightarrow TM_{0M}$ modes

For small Δn : $\sim \beta = n_2 \cdot \omega/c \approx n_1 \cdot \omega/c \sim$ linearly polarized modes of propagation: $L P_{0m}$