

EM-waves and Wave Propagation:

Reflection and Refraction on Plane Interfaces

Each medium is characterized by a unique set of ϵ_{cw} , μ_{cw} !

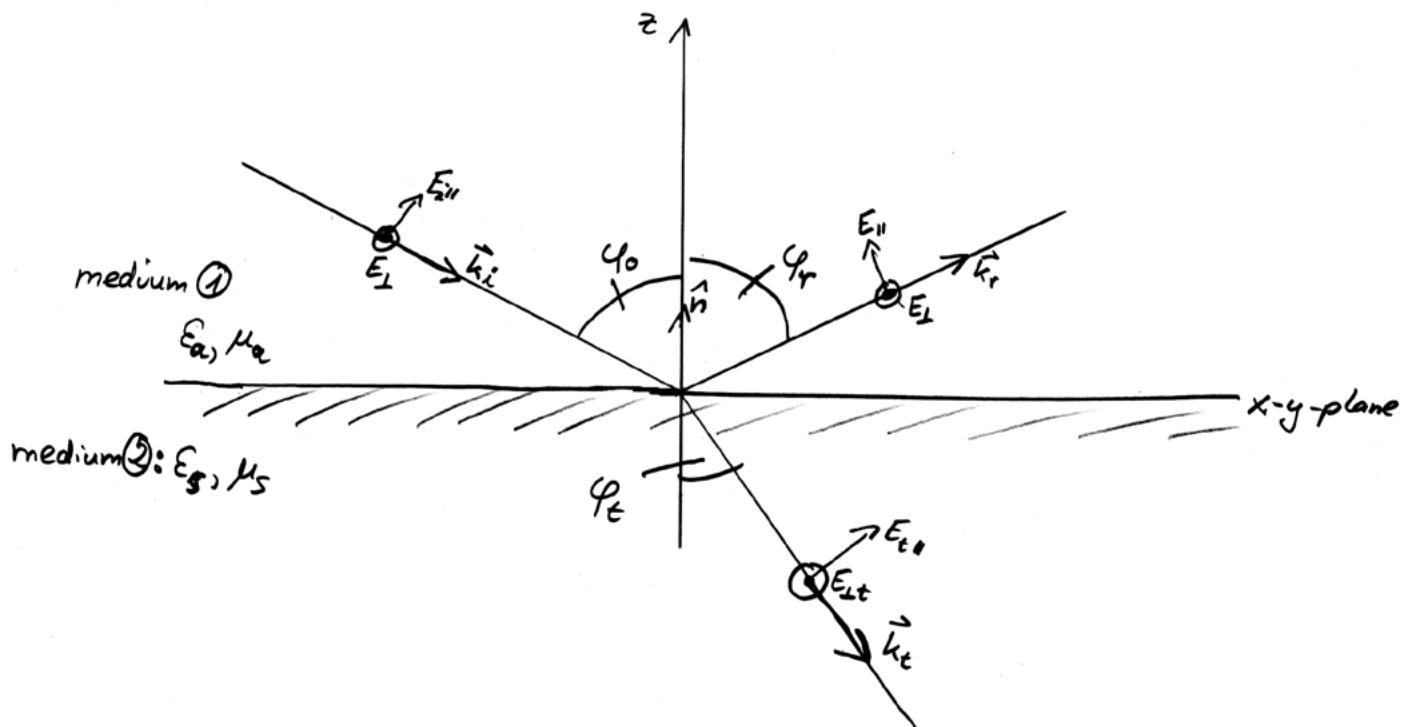
↪ entering/leaving a medium \rightarrow change of ϵ_{cw} and/or μ_{cw}

↪ Assume an incidence plane EM-wave:

$$\vec{E}_i(\vec{r}, t) = \vec{E}_{oi} \exp[i(\vec{k}_{oi}\vec{r} - \omega t)]$$

and $\vec{B}_i(\vec{r}, t) = \vec{B}_{oi} \exp[i(\vec{k}_{oi}\vec{r} - \omega t)]$

impinging on interface - separating two media, each characterized by a unique set ϵ, μ :



a.) Plane of incidence is defined by \vec{k}_i and \hat{n}

b.) Parallel polarized light: \vec{E} -vector in plane of incidence

c.) Perpendicular polarized light: \vec{E} -vector \perp plane of incidence \Rightarrow

→ The refracted and reflected EM waves are given as

$$\vec{E}_t(\vec{r}, t) = \vec{E}_{t_0} \exp[i(\vec{k}_t \cdot \vec{r} - \omega t)], \quad \vec{B}_t(\vec{r}, t) = \vec{B}_{t_0} \exp[i(\vec{k}_t \cdot \vec{r} - \omega t)]$$

$$\vec{E}_r(\vec{r}, t) = \vec{E}_{r_0} \exp[i(\vec{k}_r \cdot \vec{r} - \omega t)], \quad \vec{B}_r(\vec{r}, t) = \vec{B}_{r_0} \exp[i(\vec{k}_r \cdot \vec{r} - \omega t)]$$

Now, apply Boundary conditions:

a) spatial variation at $z=0$ are the same: phase factors $|_{z=0}$ = same

$$\rightarrow |\vec{k}_i \cdot \vec{n}|_{z=0} = |\vec{k}_r \cdot \vec{n}|_{z=0} = |\vec{k}_t \cdot \vec{n}|_{z=0}$$

$\hookrightarrow k_i \cdot \hat{y} = k_r \cdot \hat{y} = 0 \Rightarrow$ reflected & refracted wave are in the plane of incidence!

$$\hookrightarrow |\vec{k}_i| \cdot \sin \varphi_o = |\vec{k}_r| \cdot \sin \varphi_r = |\vec{k}_t| \cdot \sin \varphi_t \quad \text{and} \quad |\vec{k}_i| = |\vec{k}_t|$$

from which we get $\sin \varphi_o = \sin \varphi_r$ or $\boxed{\varphi_o = \varphi_r}$
law of reflection

$$\text{from } |\vec{k}_i| \cdot \sin \varphi_o = |\vec{k}_t| \cdot \sin \varphi_t$$

$$\rightarrow \frac{\sin \varphi_o}{\sin \varphi_t} = \frac{|\vec{k}_t|}{|\vec{k}_i|} = \frac{\omega/c \cdot \sqrt{\epsilon_r \mu_r}}{\omega/c \cdot \sqrt{\epsilon_0 \mu_0}} = \frac{n_s}{n_a}$$

or $\boxed{\frac{\sin \varphi_o}{\sin \varphi_t} = \frac{n_s}{n_a}}$ law of refraction
(Snell's Law)

b) Maxwell's boundary conditions:

① normal components of \vec{D} and \vec{B} are continuous at $z=0$

② tangential components of \vec{E} and \vec{H} are



$$\textcircled{1} \quad [\vec{D}_{i_0} + \vec{D}_{r_0} - \vec{D}_{t_0}] \cdot \hat{n} = 0 = [\epsilon_a (\vec{E}_{i_0} + \vec{E}_{r_0}) - \epsilon_s \vec{E}_{t_0}] \cdot \hat{n}$$

$$\textcircled{2} \quad [\vec{B}_{i_0} + \vec{B}_{r_0} - \vec{B}_{t_0}] \cdot \hat{n} = 0 = [\vec{k}_i \times \vec{E}_{i_0} + \vec{k}_r \times \vec{E}_{r_0} - \vec{k}_t \times \vec{E}_{t_0}] \cdot \hat{n}$$

and

$$\textcircled{3} \quad [\vec{E}_{i_0} + \vec{E}_{r_0} - \vec{E}_{t_0}] \times \hat{n} = 0$$

$$\textcircled{4} \quad [\vec{H}_{i_0} + \vec{H}_{r_0} - \vec{H}_{t_0}] \times \hat{n} = 0 = \left[\frac{1}{\mu_a} (\vec{k}_i \times \vec{E}_{i_0}) + \frac{1}{\mu_a} (\vec{k}_r \times \vec{E}_{r_0}) - \frac{1}{\mu_s} (\vec{k}_t \times \vec{E}_{t_0}) \right] \times \hat{n}$$

Let's first consider EH-wave vector \perp (perpendicular) to the plane of incidence

from $\textcircled{3}$:

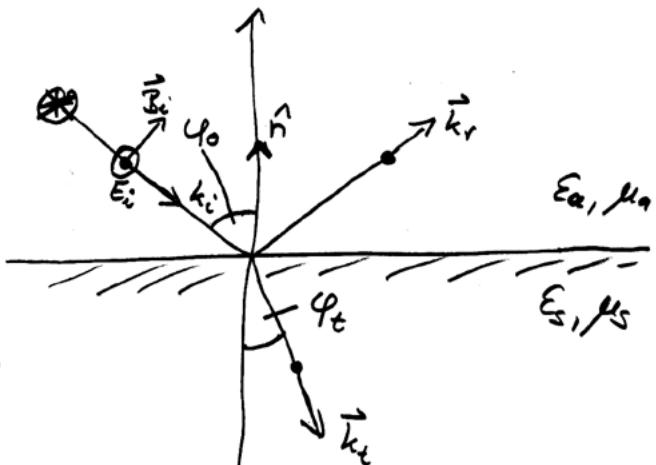
$$\vec{E}_{i_0} + \vec{E}_{r_0} - \vec{E}_{t_0} = 0$$

from $\textcircled{4}$:

$$\sqrt{\frac{\epsilon_a}{\mu_a}} (|\vec{E}_{i_0}| - |\vec{E}_{r_0}|) \cdot \cos \varphi_0 - \sqrt{\frac{\epsilon_s}{\mu_s}} E_{t_0} \cdot \cos \varphi_t = 0$$



$$t_s := \left| \frac{\vec{E}_{t_0}}{\vec{E}_{i_0}} \right|_{E_\perp} = \frac{2 \cdot \cos \varphi_0 \sqrt{\frac{\epsilon_a \mu_a}{\mu_s}}}{\sqrt{\frac{\epsilon_a \mu_a}{\mu_s}} \cdot \cos \varphi_0 - \frac{\mu_a}{\mu_s} \cdot \sqrt{\mu_s \cdot \epsilon_s - \mu_a \cdot \epsilon_a \cdot \sin^2 \varphi_0}} \quad \textcircled{5}$$



and

$$r_s := \left| \frac{\vec{E}_{r_0}}{\vec{E}_{i_0}} \right|_{E_\perp} = \frac{\sqrt{\frac{\epsilon_a \mu_a}{\mu_s}} \cdot \cos \varphi_0 - \frac{\mu_a}{\mu_s} \cdot \sqrt{\mu_s \cdot \epsilon_s - \mu_a \cdot \epsilon_a \cdot \sin^2 \varphi_0}}{\sqrt{\frac{\epsilon_a \mu_a}{\mu_s}} \cdot \cos \varphi_0 + \frac{\mu_a}{\mu_s} \cdot \sqrt{\mu_s \cdot \epsilon_s - \mu_a \cdot \epsilon_a \cdot \sin^2 \varphi_0}} \quad \textcircled{6}$$



Next, consider the electric field vector \vec{E} parallel to the plane of incidence:

The tangential components \vec{E}_t and \vec{H} continuous, demand that

$$(7) |\vec{E}_{i_0}| \cos \varphi_0 - |\vec{E}_{r_0}| \cos \varphi_0 - |\vec{E}_{t_0}| \cos \varphi_t = 0$$

$$(8) \sqrt{\frac{\epsilon_a}{\mu_a}} \cdot |\vec{E}_{i_0}| + \sqrt{\frac{\epsilon_a}{\mu_a}} |\vec{E}_{r_0}| - \sqrt{\frac{\epsilon_s}{\mu_s}} \cdot |\vec{E}_{t_0}| = 0$$

\Leftrightarrow

$$t_p := \left| \frac{\vec{E}_{t_0}}{\vec{E}_{i_0}} \right|_{E_{||}} = \frac{2 \cdot \sqrt{\mu_a \cdot \epsilon_a} \cdot \sqrt{\mu_s \cdot \epsilon_s} \cdot \cos \varphi_0}{\mu_a \cdot \epsilon_s \cos \varphi_0 + \sqrt{\mu_a \cdot \epsilon_a} \cdot \sqrt{\mu_s \cdot \epsilon_s} - \mu_a \cdot \epsilon_a \sin^2 \varphi_0} \quad (9)$$

$$r_p := \left| \frac{\vec{E}_{i_0}}{\vec{E}_{r_0}} \right|_{E_{||}} = \frac{\mu_a \cdot \epsilon_s \cdot \cos \varphi_0 - \sqrt{\mu_a \cdot \epsilon_a} \cdot \sqrt{\mu_s \cdot \epsilon_s} - \mu_a \cdot \epsilon_a \sin^2 \varphi_0}{\mu_a \cdot \epsilon_s \cos \varphi_0 + \sqrt{\mu_a \cdot \epsilon_a} \cdot \sqrt{\mu_s \cdot \epsilon_s} - \mu_a \cdot \epsilon_a \sin^2 \varphi_0} \quad (10)$$

For normal incidence ($\varphi=0$) there is no difference between parallel and perpendicular electrical field components:

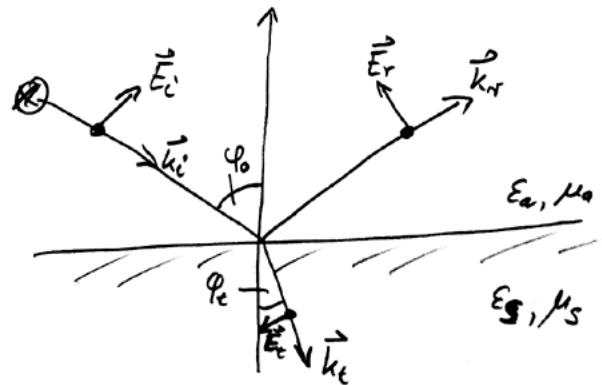
$$r_s = r_p = \frac{\sqrt{\frac{\mu_a \cdot \epsilon_s}{\mu_s \cdot \epsilon_a}} - 1}{\sqrt{\frac{\mu_a \cdot \epsilon_s}{\mu_s \cdot \epsilon_a}} + 1}$$

$$\left| \begin{array}{l} \mu_a = \mu_s = 1 \\ r_s = r_p = \frac{\sqrt{\epsilon_s} - \sqrt{\epsilon_a}}{\sqrt{\epsilon_s} + \sqrt{\epsilon_a}} = \frac{n_s - n_a}{n_s + n_a} \end{array} \right. \begin{array}{l} \text{no absorption} \end{array}$$

and

$$t_p = t_s = \frac{2}{\sqrt{\frac{\mu_a \cdot \epsilon_s}{\epsilon_a \cdot \mu_s}} + 1}$$

$$\left| \begin{array}{l} \mu_a = \mu_s = 1 \\ t_p = t_s = \frac{2 \cdot \sqrt{\epsilon_s}}{\sqrt{\epsilon_s} + \sqrt{\epsilon_a}} = \frac{2 \cdot n_a}{n_s + n_a} \end{array} \right. \begin{array}{l} \text{no absorption} \Rightarrow \end{array}$$



Equations ⑤, ⑥, ⑨ and ⑩ describe any boundary between two mathematically sharp interfaces, where either ϵ or μ changes.

The coefficients are denoted as Fresnel's Equations.

The Fresnel's coefficients are generally complex values!

The transmission (T) and Reflectivity (R) are given

by $T_p = \alpha \cdot (t_p \cdot t_p^*)$ $\alpha := \frac{T_{\epsilon_s \mu_s} - \epsilon_0 \mu_0 \sin^2 \varphi_0}{T_{\epsilon_0 \mu_0} \cdot \cos \varphi_0}$
 $T_s = \alpha \cdot (t_s \cdot t_s^*)$

and $R_s = t_s \cdot t_s^*$, $R_p = t_p \cdot t_p^*$

If there is no absorption in the media, we get from the condition that the total energy flow into the area (per time unit) has to be equal the energy flowing outwards (per time unit):

$$J_i \cdot A \cdot \cos \varphi_0 = J_r \cdot A \cdot \cos \varphi_0 + J_t \cdot A \cdot \frac{T_{\epsilon_s \mu_s} - \epsilon_0 \mu_0 \sin^2 \varphi_0}{T_{\epsilon_s \mu_s}}$$

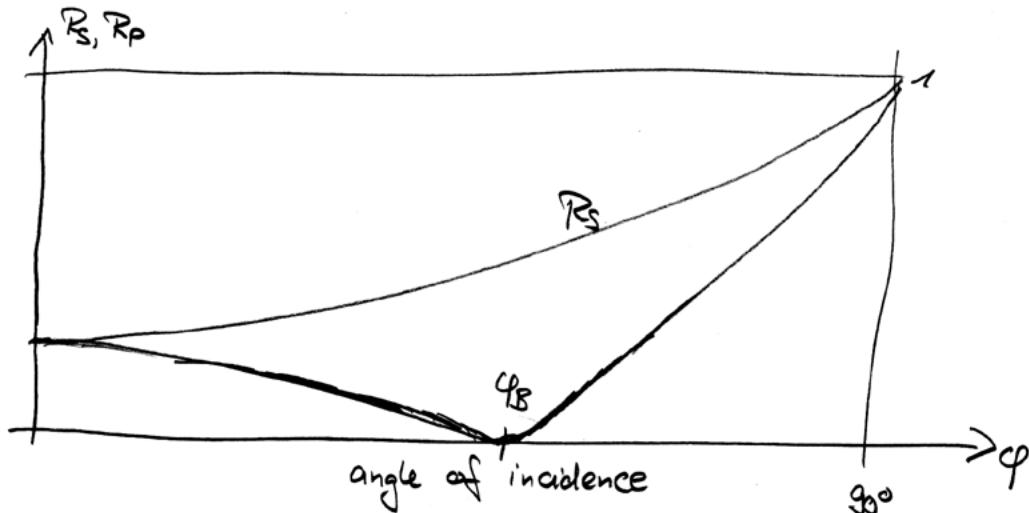
with $R = \frac{J_r}{J_i}$, $T = \frac{J_t \cos \varphi_0}{J_i \cos \varphi_0} = \frac{J_t \cdot T_{\epsilon_s \mu_s} - \epsilon_0 \mu_0 \sin^2 \varphi_0}{J_i \cdot T_{\epsilon_s \mu_s} \cdot \cos \varphi_0}$

and $R + T = 1$

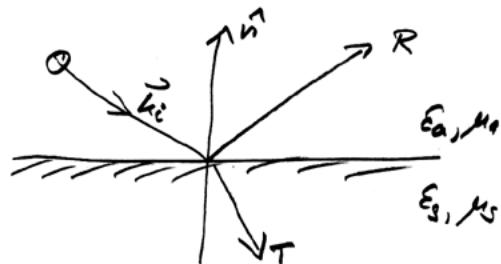
with absorption:

$$\boxed{R + T + A = 1}$$





Critical angle φ_c :



back to Snell's law: $\sqrt{\epsilon_a} \cdot \sin \varphi_i = \sqrt{\epsilon_s} \cdot \sin \varphi_t$

assume $\sqrt{\epsilon_a} > \sqrt{\epsilon_s}$: $\varphi_t = \arcsin \left[\frac{\sqrt{\epsilon_a}}{\sqrt{\epsilon_s}} \cdot \sin \varphi_i \right]$

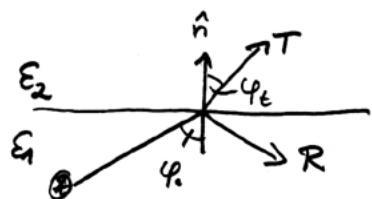
has to be ≤ 1 in order to get real φ_t

$$\sim \sin \varphi_i \leq \frac{\sqrt{\epsilon_s}}{\sqrt{\epsilon_a}}$$

$$\hookrightarrow \text{critical angle } \varphi_c := \arcsin \left[\sqrt{\epsilon_s} / \sqrt{\epsilon_a} \right]$$

$$\sqrt{\epsilon_s} = 1.5 \text{ (Glass)} \text{ and } \sqrt{\epsilon_a} = 1 \quad \sim \quad \varphi_c = \underline{41.8^\circ}$$

Brewster angle φ_B : $\varphi_B := R|_{E_{II}} = 0 \quad \text{or} \quad \frac{\partial R}{\partial \varphi}|_{E_{II}} = 0$



Transmitted and reflected rays \perp

$$\varphi_t + (90^\circ - \varphi_B) = 90^\circ$$

$$\sim \text{Snell's Law} \quad \sqrt{\epsilon_a} \sin \varphi_B = \sqrt{\epsilon_2} \cdot \cos \varphi_B \quad \sim \varphi_B = \arctan \left(\frac{\sqrt{\epsilon_2}}{\sqrt{\epsilon_a}} \right)$$